

Corrosion Study

Fourtain Quail

Corrosivity of Chlorine Dioxide on Typical Oilfield Iron

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Introduction

- Background
- Test Goals and Procedure
- Summary
- Equipment
- Fluid System
- Test Execution
- Results and Analysis





- Concern about impact of chlorine dioxide ClO2 on fluid ends and flow iron
- Current corrosion studies unrepresentative (static vs. dynamic tests)
- A test was needed that simulated flow conditions, fluid chemistry, and typical alloys used in hydraulic fracturing





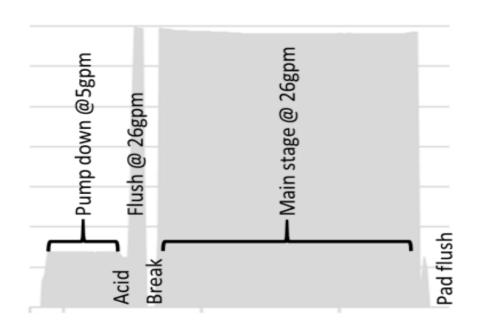




Goal

Determine the effect chlorine dioxide (ClO_2) has on common field iron used in hydraulic fracturing flow and pressure pumping equipment at

- a. Typical dose rates
- b. In a traditional slick water hydraulic fracturing fluid chemistry
- c. Using both fresh and brine water solutions
- d. In a dynamic flow environment







- Design a test to simulate flow conditions, alloys, and typical fluid chemistries
- Use fresh and brine solutions
- Mimic the steps in a conventional frac stage
- Establish a baseline using fluid systems without ClO₂, then repeat with ClO₂
- Repeat each stage and fluid system to reduce uncertainty
- Measure critical parameters to ensure consistency between stages
- Quantify corrosion rates using multiple sensors
- Analyze data to assess impact of ClO₂ on selected alloys





- Carbon steel (CS) corrosion rates were poor (1-5 mm/yr)
- Stainless steel (SS) corrosion rates were good (<0.5 mm/yr)
- Corrosion rates of CS in brine were over 30% higher than fresh
- Overall there does not appear to be any statistically significant impact of the ClO₂ in either fresh nor brine water solutions
- ClO₂ did not increase O₂ levels in any of the fluid systems used

1.0-5.0 Poor 0.5-1.0 Fair 0.1-0.5 Good



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Corrosion ranges taken from Corrosion Engineering (1986) by Mars G. Fontana, McGraw-Hill Book Co., NY, ISBN: 0-07-021463-8

Test Fixture and Flow Plan

HF Fluid Simulation Flow Loop				Sensor Isolation SI3				4" Pipe		¾″ Pipe		Flow Loop	
Flow Loop	pH /ORP Sensor Conductivity / Temperatur	<u></u>		<u>, </u>		T9D	Stage	Flow	Velocity	Flow	Velocity	Run Time	Volume
	Sensor Turbidity 0-100 PSI]		Sensor Throttle SB2	•	To T9 Dispo	Simulation	(BPM)	(FPS)	(GPM)	(FPS)	(Minutes)	(gal)
DO (0 ₂) Sensor				Drain/Sample Line DL2 T9R Master Recirc			Water only	2.0	2.1	3.0	2.2	3.0	9.0
	Velocity and Flow Rate Meter			oon Steel Spools			Pump Down	3.5	3.8	5.0	3.6	32.0	160.0
3" PVC Reduction Header Drain/Sample Line DL3 P1S						Break	3.0	3.2	4.5	3.3	2.0	9.0	
						Acid Phase	7.0	7.5	10.5	7.3	1.0	10.5	
						Flush	17.5	18.8	26.0	18.8	6.0	156.0	
Drain/Sample Line DL1					_		Pause					5.00	
T1S 🗗 T1R 🗗 T2S 🗗 T2R 🗗 T3	5 🖸 T3R 💽 T4S 🔂	T4R 🗗 🛛 T5S 🗗 T5R 🗗	T6S 🔤 T6R 💽	T7S 🚭 T7R 🚭	T85 🚭 T8R 🚭		Water Pad	17.5	18.8	26.0	18.8	5.0	130.0
Tank 1 HCI 7.5% Fresh		nk 4 Tank 5 esh 60/40 blend	Tank 6 60/40 blend	Slurry @ 1.0 ppg	Tank 8 Fresh Water		Slurry	17.5	18.8	26.0	18.8	100.0	2,600.0
+ CI SI (CIO2)	SI + FR Slurry (CIO2) @ 1.0 p +SI + F	0 ppg (ClO2)	SI + FR (CIO2)				Flush	17.5	18.8	26.0	18.8	6.0	156.0
		+ FR 102)		+SI + FR (CIO2)			Total					160.0	















Instrumentation

- Chlorine Dioxide (ClO₂):Kuntze Zircon[™] DIS Sensor Model No:231512110
- Dissolved Oxygen (DO): Endress+Hauser: Oxymax COS61D Model No: COS61D-1014/0
- Conductivity: Endress+Hauser: Condumax CLS21D Model No: CLS21D-C1N1
- Turbidity: Endress+Hauser: Turbimax CUS51D Model No: CUS51D-10V6/0
- pH & ORP: Endress+Hauser: Memosens CPS16D Model No: CPSD16D-1009/0
- Pressure: Burkert Type 8323 S 0-200psig
- Flow: Endress+Hauser ProMass 100 Flowmeter







Corrosion Monitoring

Three methods of measuring corrosion were used



LPR Probes using 304SS, 316SS, and 4130CS electrodes



Seven cylinder coupons (4130CS, 4140CS, 4150CS, 4340CS, 17-4SS, 304SS, 316SS)



7.3ft of 0.75" ID tubular components (CS, 304SS)



Test Plan – Fluid Summary

- The simulated frac fluid consisted of friction reducer, scale inhibitor, and 100 mesh sand at 1ppg
- The acid phase used 7.5% HCl with corrosion inhibitor @ 2.5 gpt
- On Day 3 and 4 water was treated with ClO₂ to a 5ppm residual before beginning each stage

Scale Inhibitor @ 0.25gpt SC-30 sourced from X-CHEM (0.25gpt) 0.5 – 1.5% Sodium hydroxide Friction Reducer @ 1.0gpt TFR-24La sourced from Tucker Energy Services (1.0gpt) 15-20% Petroleum Distillate Ammonium Chloride < 1% Oleic Acid Diethanolaide <1% 50 - 60% Water **Corrosion Inhibitor @ 2.5gpt** TCA-6038 sourced from X-CHEM (2.5gpt) 50 - 70% Methanol 20-30% Pyridine Benzyl Quaternary Ammonium Chloride 5-10% Water



Test Summary

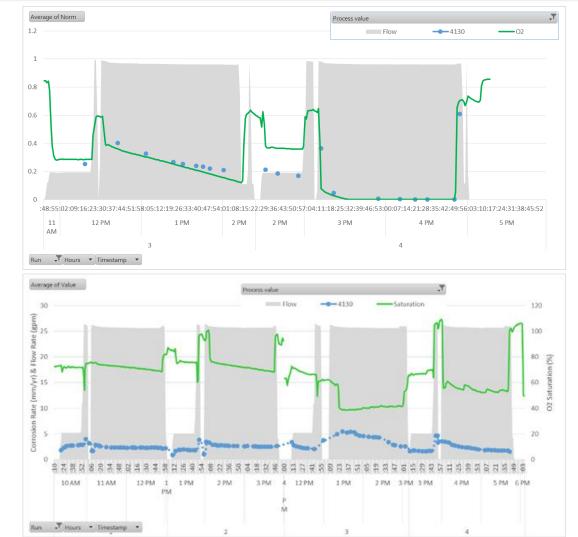
- Testing conducted on Monday, July 24, 2017 through Thursday, July 27, 2017
- Four days of testing divided into two simulated frac stages per day
- Each stage was approximately 3 hours and consisted of six phases
 ①pump down ②acid ③flush ④pad
 ⑤proppant ⑥final flush
- Flow loop was flushed each day and left full to keep sensors wet.





Test Plan B

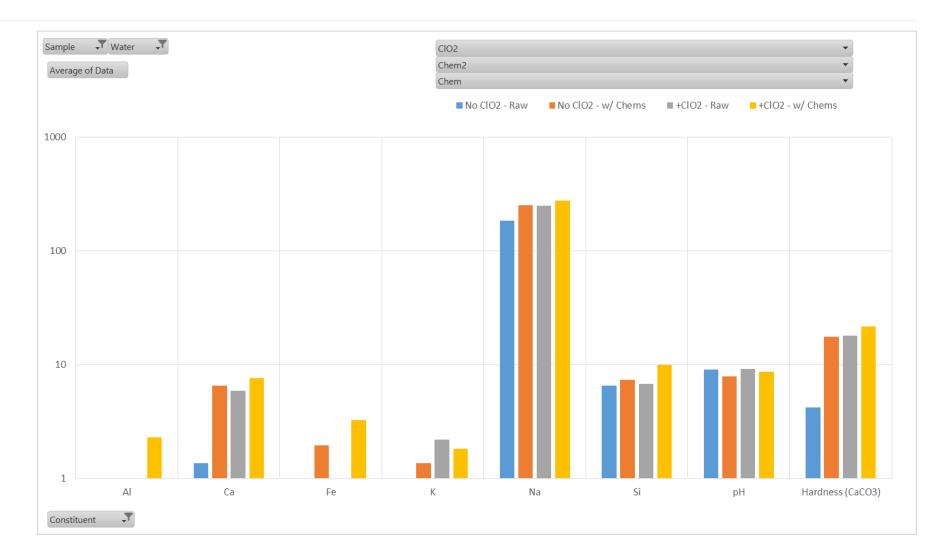
- O₂ in Slurry Tank dropped unexpectedly
- Corrosion rates were significantly lower
- Corrosion data was compromised resulting in the loss of a baseline
- A "recycle" of the 60/40 test was needed
- "Fresh" produced water was acquired
- Brine test was run again on Oct 3-4
- O₂ Levels were consistent





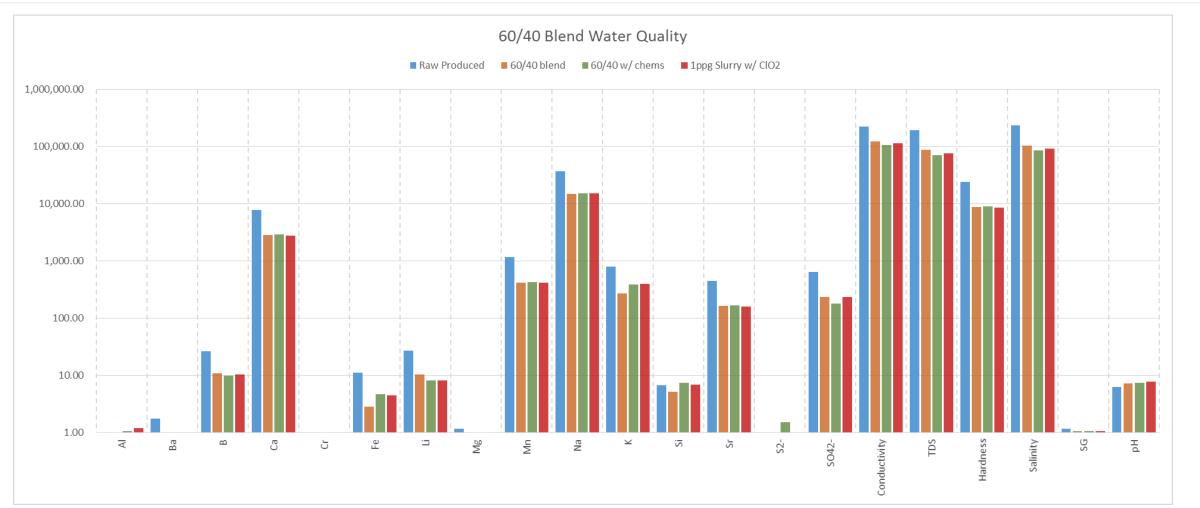
Fresh Water Quality

 Elements with concentrations < 1.0 are not shown





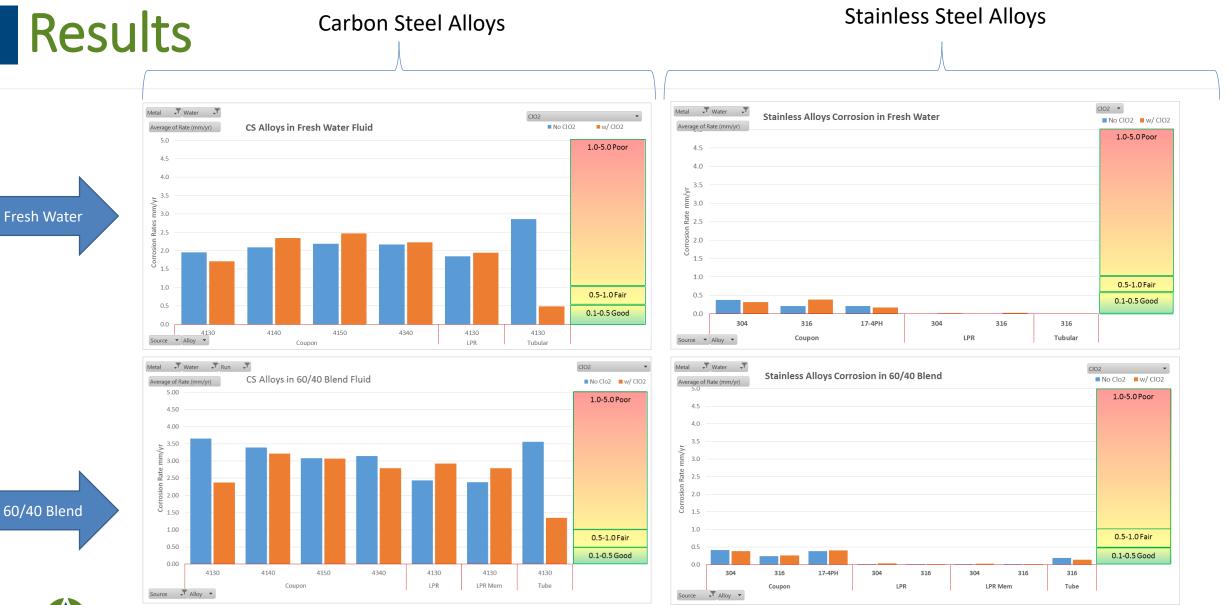
Produced Water Quality





Results and Analysis



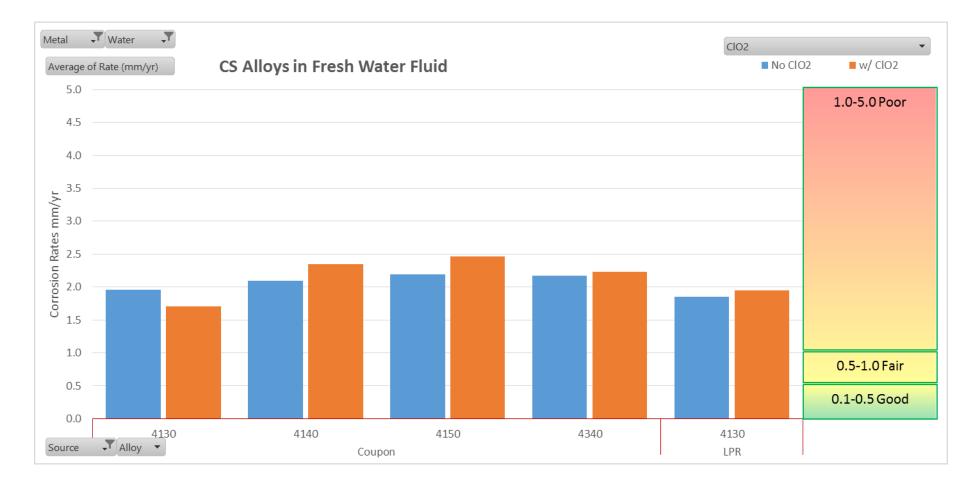


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Carbon Steel Individual Coupons (Fresh Water)





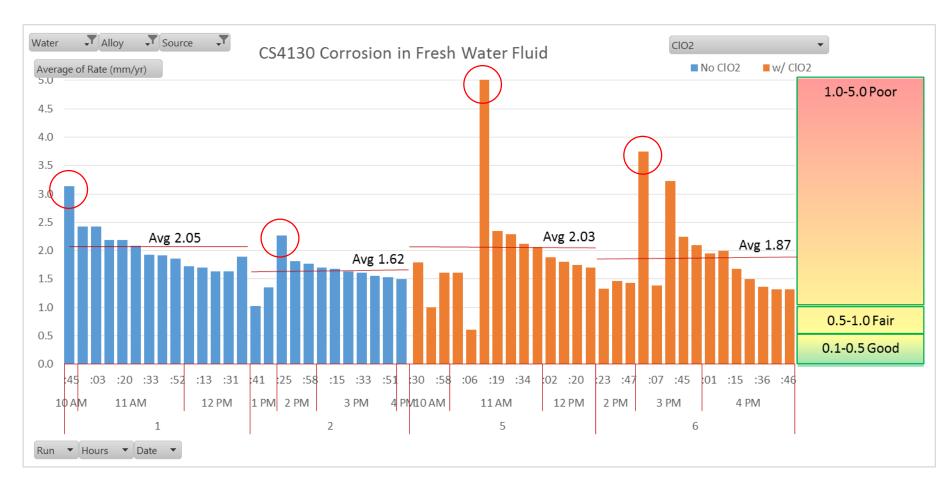
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CS4130 Alloy (Fresh Water)

The spikes in corrosion () are a reaction to the acid pad, but rates dropped back to a lower equilibrium each time.





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Corrosion ranges taken from Corrosion Engineering (1986) by Mars G. Fontana, McGraw-Hill Book Co., NY, ISBN: 0-07-021463-8

Carbon Steel Coupons Averages (A&B) (60/40)



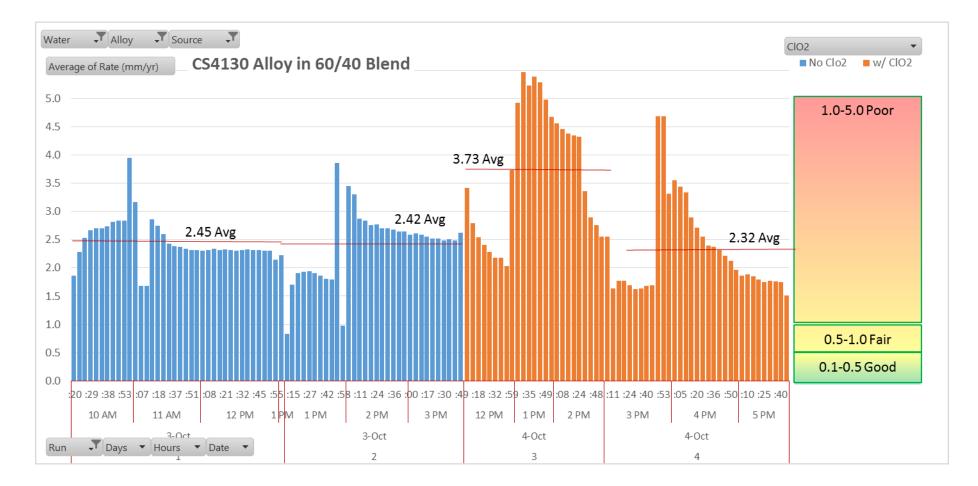


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CS4130 Alloy in 60/40 Blend



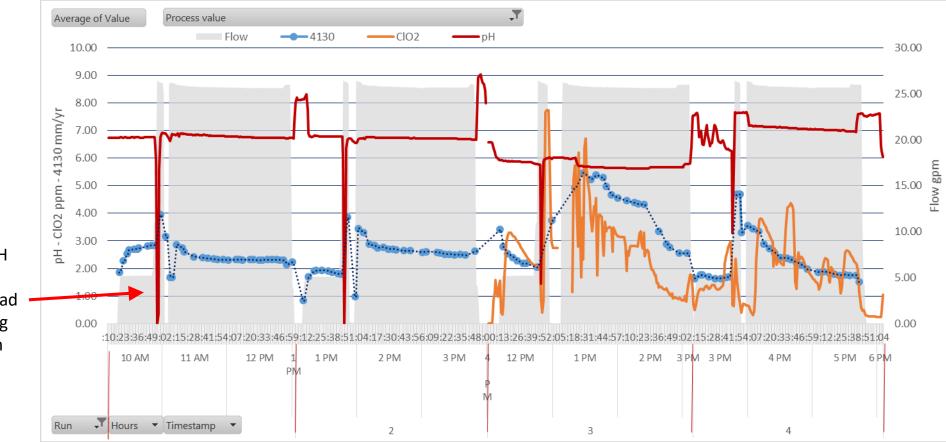


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4130 Corrosion in 60/40 Blend w/ ClO2 Residuals & pH

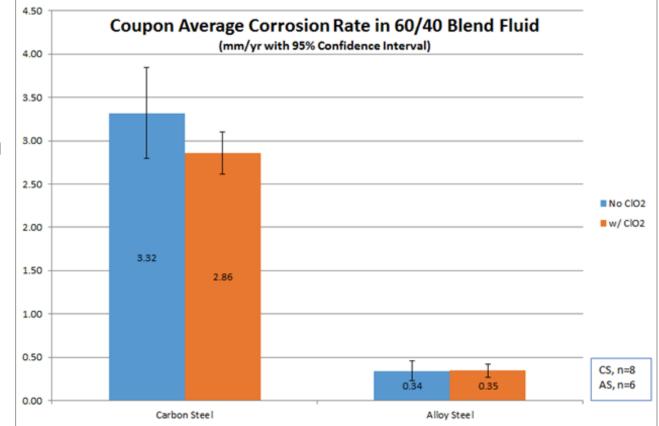


Note the low pH spikes resulting from the acid pad residual flushing thru the system



Carbon Steel Statistical Analysis

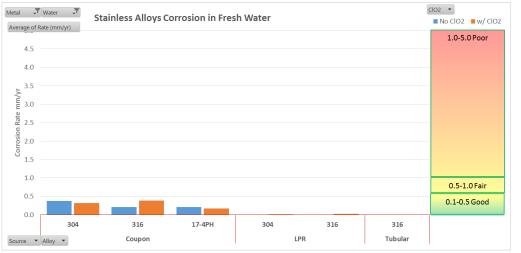
- Statistical analysis of the corrosion coupon data in the 60/40 blend shows no statistically significant difference with or without addition of ClO₂ in either group.
- This can be seen graphically in the overlap of confidence intervals.

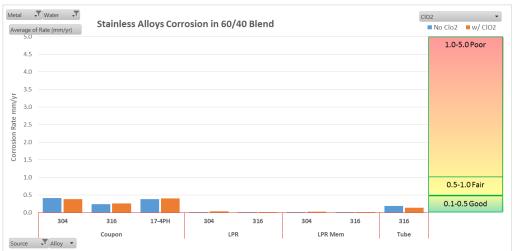




Stainless Alloys

- Corrosion of the stainless alloys was consistently in the excellent to good range
- No statistically significant impact of the ClO₂ in either fresh nor brine water solutions
- The average of both observed and memory LPR data was <0.1 mm/yr while coupon corrosion rates were <0.29 mm/yr in fresh water and <0.35 mm/yr in the 60/40 blend







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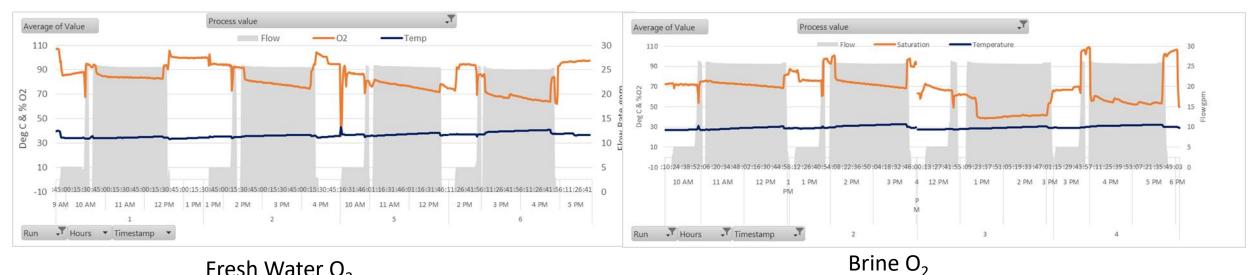
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Conclusions



Conclusions – Water Chemistry

- ClO₂ did not change water chemistry
- ClO₂ did not increase O₂ saturation
- Excess acid in poor quality ClO₂ effected carbon steel when pH < 5.8 and ClO₂ 3. residuals > 3.0





Fresh Water O₂

Conclusions - Corrosivity

Fresh Water	Brine Water
	A The explication of CIO, head way (little

- The application of ClO₂ had very little effect on stainless alloys
- Carbon steel corrosion rates showed some slight increase but less than 4% overall
- The application of ClO₂ had very little effect on stainless alloys
- Carbon steel (CS) corrosion rates were over 30% higher than fresh water
- CS exposed to low pH and high ClO₂ residuals appears more susceptible to corrosion
- Adding ClO₂ shows no detrimental impact over a statistically significant population of CS samples and test runs



Acknowledgements

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Flow loop fabrication and operational support

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Water Analysis

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Metal Analysis

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- ERCO Worldwide



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<u>ClO₂ application and technical support</u>

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 - Pete Garrison
 - Alan Burke
 - Scott Glynn
 - Bill Hulsman



Questions?

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